

Homework #2
Solutions

Problem 1. Following the hint, we write

$$\nabla = \mathbf{t} \frac{\partial}{\partial s} + \mathbf{n} \frac{\partial}{\partial n}$$

near the boundary $C = \partial\Omega$. Note first that

$$\nabla u|_C = \mathbf{t} \frac{\partial u}{\partial s} + \mathbf{n} \frac{\partial u}{\partial n} \Big|_C = \mathbf{n} \epsilon_w$$

since $u \equiv 0$ on C and thus $\partial u / \partial s \equiv 0$ as well. For the Laplacian Δu we can likewise calculate

$$\begin{aligned} \Delta u &= \left(\mathbf{t} \frac{\partial}{\partial s} + \mathbf{n} \frac{\partial}{\partial n} \right) \cdot \left(\mathbf{t} \frac{\partial u}{\partial s} + \mathbf{n} \frac{\partial u}{\partial n} \right) \\ &= \left(\frac{\partial^2 u}{\partial s^2} + \mathbf{t} \cdot \frac{\partial \mathbf{t}}{\partial s} \frac{\partial u}{\partial s} + \mathbf{n} \cdot \frac{\partial \mathbf{t}}{\partial n} \frac{\partial u}{\partial s} \right) \\ &\quad + \left(\mathbf{t} \cdot \frac{\partial \mathbf{n}}{\partial s} \frac{\partial u}{\partial n} + \frac{\partial^2 u}{\partial n^2} \right) \end{aligned}$$

where the first parenthetical expression arises from the divergence of $\mathbf{t} \partial u / \partial s$ and the second expression arises from $\mathbf{n} \partial u / \partial n$. We have made use of $\mathbf{t} \cdot \mathbf{n} = 0$ to eliminate some terms. If we now consider the restriction to the wall, then

$$\Delta u|_C = \mathbf{t} \cdot \frac{\partial \mathbf{n}}{\partial s} \frac{\partial u}{\partial n} + \frac{\partial^2 u}{\partial n^2} \Big|_C$$

since again $\partial u / \partial s = \partial^2 u / \partial s^2 \equiv 0$ on C .

Recalling also the relation

$$\mathbf{t} \cdot \frac{\partial \mathbf{n}}{\partial s} = -\mathbf{n} \cdot \frac{\partial \mathbf{t}}{\partial s}$$

obtained by differentiating $\mathbf{t} \cdot \mathbf{n} = 0$, we then use the result from the hint

$$\frac{\partial \mathbf{t}}{\partial s} = \pm \kappa \mathbf{n}$$

which follows from the Frenet-Serret equations and our definition of \mathbf{n} as pointing inward to Ω . Thus,

$$\Delta \mathbf{u} \Big|_C = \mp \kappa \frac{\partial \mathbf{u}}{\partial n} + \frac{\partial^2 \mathbf{u}}{\partial n^2} \Big|_C.$$

and using the Navier-Stokes equation on the boundary

$$\nu \Delta \mathbf{u} - \nabla p = \mathbf{0} \text{ on } C,$$

we obtain

$$\nu \frac{\partial^2 \mathbf{u}}{\partial n^2} = \pm \kappa \boldsymbol{\tau}_w + \nabla p \text{ on } C.$$

We have set $\boldsymbol{\tau}_w = \nu \boldsymbol{\epsilon}_w$. Now taking the tangential component

$$\nu \frac{\partial^2 u_t}{\partial n^2} = \pm \kappa \tau_w + \frac{\partial p}{\partial s}$$

whereas the normal component gives

$$\nu \frac{\partial^2 u_n}{\partial n^2} = \frac{\partial p}{\partial n},$$

since $\mathbf{n} \cdot \boldsymbol{\tau}_w = 0$.

Problem 2. (a) From the defining equations

$$\dot{x} = u, \quad \dot{y} = v$$

we obtain

$$\dot{x}_\alpha = u_x x_\alpha + u_y y_\alpha, \quad \alpha = \xi, \eta$$

$$\dot{y}_\alpha = v_x x_\alpha + v_y y_\alpha, \quad \alpha = \xi, \eta$$

by taking derivatives of both sides with respect to either ξ or η .

In that case,

$$\begin{aligned} & \frac{d}{dt} (x_\xi y_\eta - x_\eta y_\xi) \\ &= (u_x x_\xi + \cancel{u_y y_\xi}) y_\eta + x_\xi (v_x \cancel{x_\eta} + v_y y_\eta) \\ & \quad - (u_x x_\eta + \cancel{u_y y_\eta}) y_\xi - x_\eta (v_x \cancel{x_\xi} + v_y y_\xi) \\ &= (u_x + v_y) (x_\xi y_\eta - x_\eta y_\xi) \end{aligned}$$

Note that at the initial time $x_\xi = y_\eta = 1$, $x_\eta = y_\xi = 0$

so that

$$x_\xi y_\eta - x_\eta y_\xi \Big|_{t=0} = 1.$$

Since this linear equation for $(x_\xi y_\eta - x_\eta y_\xi)$ has a unique solution, it follows that

$$u_x + v_y \equiv 0 \quad \text{iff} \quad x_\xi y_\eta - x_\eta y_\xi \equiv 1.$$

(b) Note that

$$\begin{bmatrix} \xi_x & \xi_y \\ \eta_x & \eta_y \end{bmatrix} = \begin{bmatrix} x_\xi & x_\eta \\ y_\xi & y_\eta \end{bmatrix}^{-1}$$

since $(\xi(x,y), \eta(x,y))$ is the inverse map to $(x(\xi,\eta), y(\xi,\eta))$.

However, because

$$\begin{vmatrix} x_\xi & x_\eta \\ y_\xi & y_\eta \end{vmatrix} = x_\xi y_\eta - x_\eta y_\xi \equiv 1$$

$$\begin{bmatrix} x_\xi & x_\eta \\ y_\xi & y_\eta \end{bmatrix} = \begin{bmatrix} y_\eta & -x_\eta \\ -y_\xi & x_\xi \end{bmatrix}$$

and thus we read off

$$\xi_x = y_\eta, \quad \xi_y = -x_\eta$$

$$\eta_x = -y_\xi, \quad \eta_y = x_\xi.$$

(c) We note that by the chain rule and the equation $\dot{x} = u$

$$\begin{aligned} \ddot{x} &= \frac{d}{dt} u(x,y,t) \\ &= u_t + \dot{x} u_x + \dot{y} u_y \\ &= u_t + u u_x + v u_y \end{aligned}$$

Next, we use the x-momentum equation of the Prandtl theory to infer that

$$\ddot{x} = -p_x + \partial_y^2 u$$

We next use

$$\begin{aligned} \frac{\partial}{\partial y} &= \frac{\partial \xi}{\partial y} \frac{\partial}{\partial \xi} + \frac{\partial \eta}{\partial y} \frac{\partial}{\partial \eta} \\ &= -x_\eta \frac{\partial}{\partial \xi} + x_\xi \frac{\partial}{\partial \eta} \end{aligned}$$

by exploiting the relations from part (b). However,

$$u = \dot{x}$$

and

$$\frac{\partial^2}{\partial y^2} = \left(x_\eta \frac{\partial}{\partial \xi} - x_\xi \frac{\partial}{\partial \eta} \right)^2$$

so that we obtain the final result that

$$\ddot{x} = -p_x(x) + (x_\eta \frac{\partial}{\partial \xi} - x_\xi \frac{\partial}{\partial \eta})^2 \dot{x}.$$

This is a second-order in time, nonlinear PDE for the Lagrangian flow map $x(\xi, \eta)$. The other component $y(\xi, \eta)$ can be obtained from the relation

$$x_\xi y_\eta - x_\eta y_\xi \equiv 1.$$

QED

Problem 3. (a) First we note that from $\mathbf{n} = \nabla d(\mathbf{x})$

$$\begin{aligned}\frac{\partial \mathbf{n}}{\partial n} &:= (\mathbf{n} \cdot \nabla) \mathbf{n} = \mathbf{n} \cdot (\nabla \nabla d) \\ &= n_i \nabla n_i \quad (\text{summing over repeated } i) \\ &= \nabla \left(\frac{1}{2} n_i n_i \right) \\ &= 0\end{aligned}$$

since $\mathbf{n} \cdot \mathbf{n} = 1$. Then using the above

$$\mathbf{n} \cdot \boldsymbol{\epsilon}_w = \mathbf{n} \cdot \frac{\partial \mathbf{u}}{\partial n} \Big|_S = \frac{\partial}{\partial n} (\mathbf{n} \cdot \mathbf{u}) \Big|_S = 0$$

since by incompressibility and stick b.c.

$$\frac{\partial u_n}{\partial n} = -\nabla_S \cdot \mathbf{u}_S \equiv 0 \quad \text{on } S.$$

(b) We begin with

$$\begin{aligned}\boldsymbol{\tau}_w &= 2\nu \mathbf{S} \cdot \mathbf{n} = \nu \left(\frac{\partial \mathbf{u}}{\partial n} + \nabla u_j n_j \right) \Big|_S \\ &= \nu \frac{\partial \mathbf{u}}{\partial n} + \nu \nabla (u_j n_j) \Big|_S\end{aligned}$$

since $u_j \nabla n_j \equiv 0$ on S . However, by part (a)

$$\frac{\partial}{\partial n} (u_j n_j) = \frac{\partial u_n}{\partial n} = 0$$

and

$$\nabla_S u_n \equiv 0 \quad \text{on } S$$

because of the stick b.c. Thus, we see that

$$\tau_w = v \frac{\partial u}{\partial n} = v \epsilon_w \text{ on } S.$$

For the second relation we perform a similar calculation

$$\begin{aligned} (\omega \times n)_i &= \epsilon_{ijk} \omega_j n_k \\ &= \epsilon_{ijk} \epsilon_{jlm} \partial_l u_m n_k \\ &= (\delta_{im} \delta_{kl} - \delta_{il} \delta_{km}) \partial_l u_m n_k \\ &= (n_k \partial_k) u_i - (\partial_i u_k) n_k \\ &= \frac{\partial u_i}{\partial n} - 0 \quad \text{since } (\partial_i u_k) n_k = \partial_i (u_k n_k) = 0 \\ &\quad \text{as above} \end{aligned}$$

or

$$\omega \times n = \frac{\partial u}{\partial n} = \epsilon_w.$$

Thus,

$$\tau_w = v \epsilon_w = v \omega \times n.$$

(c) We note that

$$n_i K_{ij} = -\frac{\partial n_j}{\partial n} = 0$$

from part (a), while

$$K_{ij} n_j = -(\partial_i n_j) n_j = -\partial_i \left(\frac{1}{2} n_j n_j \right) = 0$$

since $n_j n_j \equiv 1$.

(d) Incompressibility implies that

$$\frac{\partial u_n}{\partial n} + \nabla_s \cdot \mathbf{u}_s = 0$$

Taking a second derivative $\partial/\partial n$ then gives

$$-\frac{\partial^2 u_n}{\partial n^2} = \nabla_s \cdot \frac{\partial \mathbf{u}_s}{\partial n} = \nabla_s \cdot \boldsymbol{\epsilon}_w \text{ on } S.$$

Next we use $\boldsymbol{\epsilon}_w = \boldsymbol{\omega}_w \times \mathbf{n}$ from part (b) and a vector calculus identity to obtain

$$\begin{aligned} \nabla_s \cdot \boldsymbol{\epsilon}_w &= \nabla_s \cdot (\boldsymbol{\omega}_w \times \mathbf{n}) \\ &= (\nabla_s \times \boldsymbol{\omega}_w) \cdot \mathbf{n} - \boldsymbol{\omega}_w \cdot (\nabla \times \mathbf{n}) \end{aligned}$$

Note that

$$\boldsymbol{\omega}_w \cdot (\nabla \times \mathbf{n}) = \epsilon_{ijk} \omega_i \partial_j n_k = -\epsilon_{ijk} \omega_i K_{jk}.$$

However, $\boldsymbol{\omega}$ is tangent to S and can thus be written as $\boldsymbol{\omega} = \alpha \mathbf{e} + \beta \mathbf{f}$ where \mathbf{e}, \mathbf{f} is a basis for the tangent space.

Likewise, from part (c) we see that

$$\nabla \mathbf{n} = \gamma \mathbf{e}\mathbf{e} + \delta \mathbf{e}\mathbf{f} + \epsilon \mathbf{f}\mathbf{e} + \theta \mathbf{f}\mathbf{f}$$

so that $\epsilon_{ijk} \omega_i \partial_j n_k \equiv 0$. It follows that

$$\nabla_s \cdot \boldsymbol{\epsilon}_w = (\nabla_s \times \boldsymbol{\omega}_w) \cdot \mathbf{n} = (\mathbf{n} \times \nabla_s) \cdot \boldsymbol{\omega}_w.$$

QED

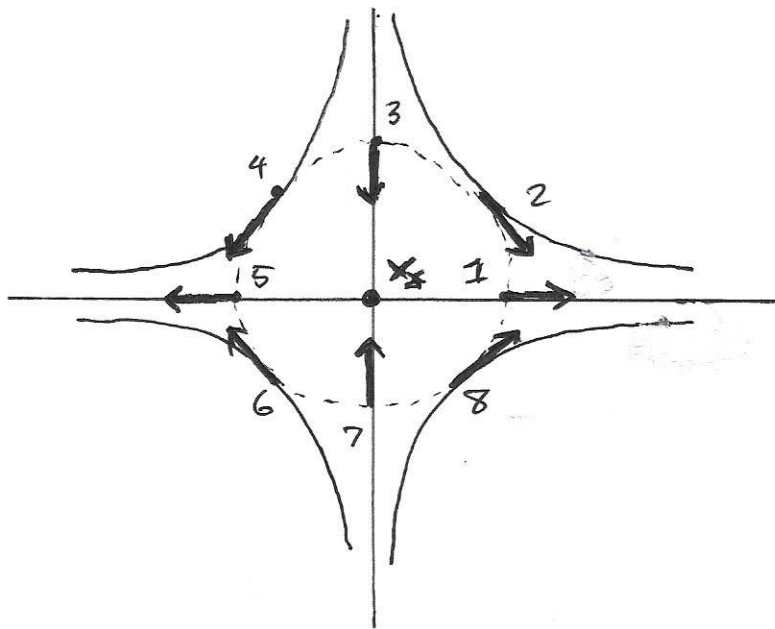
Problem 4. (a) The linearization at the fixed point $A = \nabla_{xx} V(x_*)$ is

$$A = \begin{bmatrix} 1 & 0 \\ 0 & -1 \end{bmatrix}$$

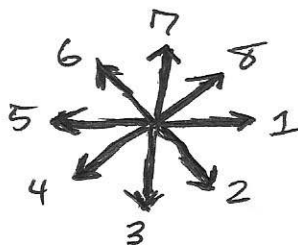
which has $\det A = -1 < 0$ and is thus a saddle point.
 In fact, the y -axis is the stable manifold and the x -axis is the unstable manifold. Note also that

$$\frac{d}{dt}(xy) = \dot{x}y + x\dot{y} = x \cdot y + x \cdot (-y) = 0$$

so that phase orbits are given by hyperbolae with $xy = \text{const.}$
 The phase portrait looks like:



On a circle around the critical point at the origin we indicate the unit vectors \hat{u} at eight points numbered counterclockwise. These are the vectors



Clearly, these vectors rotate once clockwise so that

$$\text{Index} = -1.$$

(b) The linearization at the fixed point is

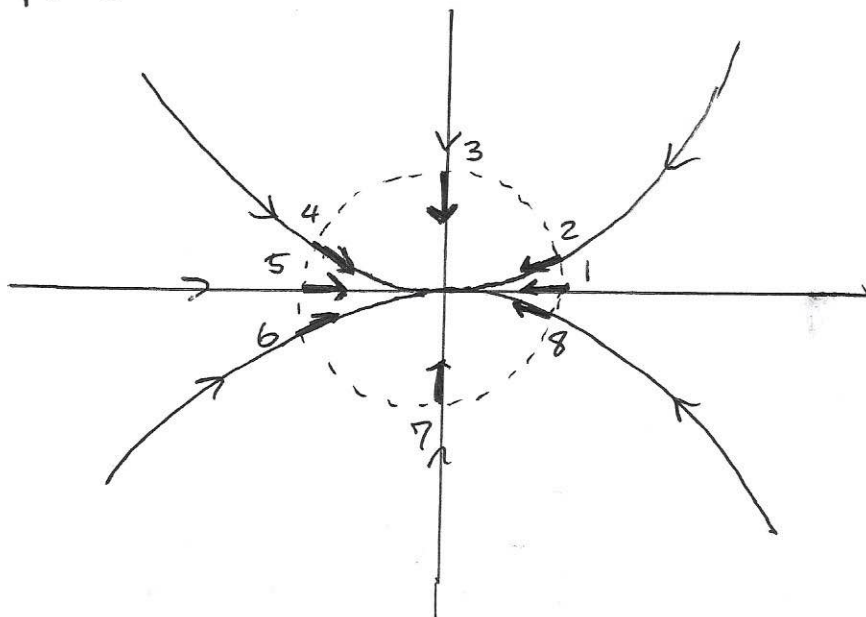
$$A = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix}$$

which has $\det A = 2 > 0$, $\text{tr} A = -3 < 0$, $\text{Dis} A = 9 - 8 = 1 > 0$
so that the critical point is a stable node. Note that

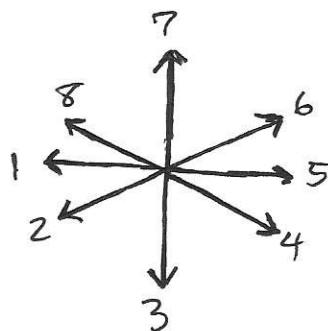
$$\begin{aligned} \frac{d}{dt} \left(\frac{y}{x^2} \right) &= \frac{y}{x^3} (\dot{y}x - 2y\dot{x}) \\ &= \frac{y}{x^3} (-2yx + 2yx) = 0 \end{aligned}$$

so that phase orbits are parabolae $y = Cx^2$, $C = \text{const.}$

The phase portrait is:



The vector plot is now



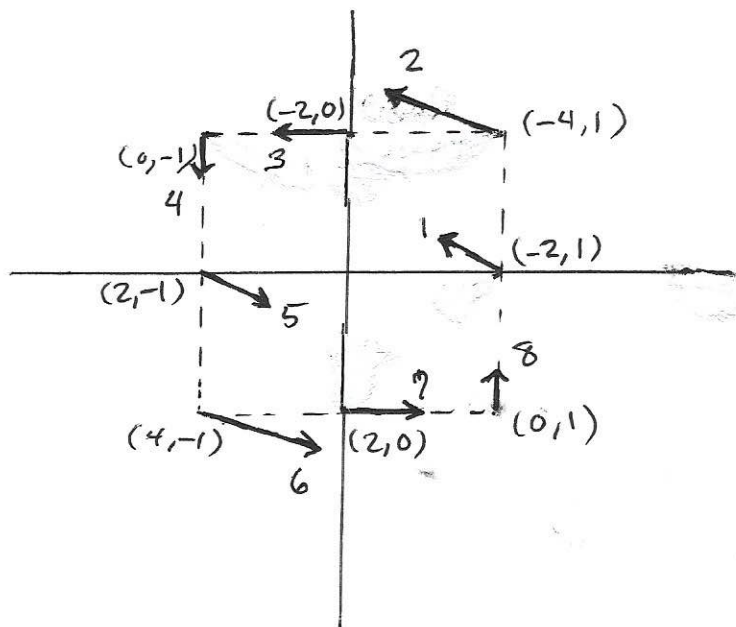
So that \vec{u} rotates once counterclockwise and thus

$$\text{Index} = +1$$

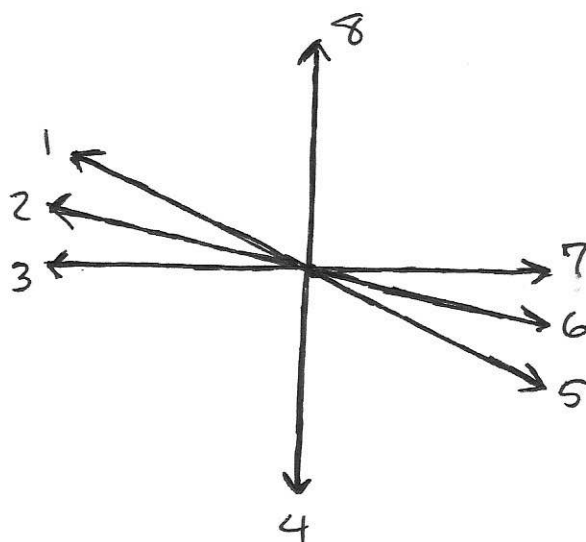
(c) The linearization at the fixed point is

$$A = \begin{bmatrix} -2 & -2 \\ 1 & 0 \end{bmatrix}$$

So that $\det A = 2 > 0$, $\text{tr} A = -2 < 0$, $\text{dis} A = 4 - 8 = -4 < 0$ and thus the critical point is a stable spiral. It is easiest here to consider a square box around the critical point



Which yields the vector plot



so that again \hat{u} rotates once counterclockwise and thus

$$\text{Index} = +1.$$

Note that the continuity of the index under changes of the contour C can be inferred from the integral expression

$$\text{Index}(f, x_*) = \frac{1}{2\pi} \oint_C \frac{f_x df}{\|f\|^2}.$$

Since the index is continuous in C but also integer-valued, it does not change under deformations of C , as long as these do not hit the critical point x_* . Thus, the value is independent of the particular contour C selected to encircle the critical point.

Problem 5, (a) Note by change of variable $s \rightarrow \bar{y} = sy$ that

$$\begin{aligned}\bar{u}_y(x, y, t) &:= \int_0^1 u_y(x, sy, t) ds \\ &= \frac{1}{y} \int_0^y u_y(x, \bar{y}, t) d\bar{y} \\ &= \frac{1}{y} [u(x, y, t) - u(x, 0, t)] \\ &= \frac{1}{y} u(x, y, t) \quad \text{since } u(x, 0, t) = 0\end{aligned}$$

and thus

$$u(x, y, t) = \bar{u}_y(x, y, t) y.$$

Similarly, we change the variable $s \rightarrow \bar{y} = ry$ to obtain

$$\begin{aligned}\int_0^1 v_{yy}(x, rsy, t) r ds \\ &= \frac{1}{y} \int_0^{ry} v_y(x, \bar{y}, t) d\bar{y} \\ &= \frac{1}{y} [v_y(x, ry, t) - v_y(x, 0, t)] \\ &= \frac{1}{y} v_y(x, ry, t)\end{aligned}$$

since $v_y(x, 0, t) = -u_x(x, 0, t) = 0$ by incompressibility and stick b.c.

In that case, using the definition of $\overline{v_{yy}}(x, y, t)$

$$\begin{aligned} & \int_0^1 \int_0^1 v_{yy}(x, ry, t) 2r \, dr \, ds \\ &= \frac{2}{y} \int_0^1 v_y(x, ry, t) \, dr \quad r \rightarrow \bar{y} = ry \\ &= \frac{2}{y^2} \int_0^y v_y(x, \bar{y}, t) \, d\bar{y} \\ &= \frac{2}{y^2} [v(x, y, t) - v(x, 0, t)] \\ &= \frac{2}{y^2} v(x, y, t) \end{aligned}$$

and thus

$$v(x, y, t) = \frac{1}{2} \overline{v_{yy}}(x, y, t) y^2.$$

(b) By incompressibility

$$\begin{aligned} 0 &= \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = \frac{\partial}{\partial x} (\bar{u}_y y) + \frac{\partial}{\partial y} \left(\frac{1}{2} \overline{v_{yy}} y^2 \right) \\ &= y \cdot \bar{u}_{y,x} + \frac{1}{2} y^2 \cdot \overline{v_{yy,y}} + y \cdot \overline{v_{yy}} \end{aligned}$$

$$\Rightarrow \bar{u}_{y,x} + \overline{v_{yy}} + \frac{1}{2} \overline{v_{yy,y}} = 0.$$

(c) Finally, $x = \gamma + y F(y, t)$ is a material curve if and only if each point of it evolves according to the equations

$$\begin{aligned}\dot{x} &= u = \bar{u}_y y \\ \dot{y} &= v = \frac{1}{2} \bar{v}_{yy} y^2\end{aligned}$$

Substituting into the first equation yields by chain rule

$$\begin{aligned}y F_t(y, t) + \dot{y} F(y, t) + y \dot{y} F_y(y, t) \\ &= \bar{u}_y(x, y, t) y \\ &= \bar{u}_y(\gamma + y F, y, t) y\end{aligned}$$

so that

$$F_t(y, t) = \bar{u}_y(\gamma + y F, y, t) - \frac{\dot{y}}{y} (F + y F_y).$$

Now substituting from the second equation for \dot{y} gives

$$\begin{aligned}F_t(y, t) &= \bar{u}_y(\gamma + y F, y, t) \\ &\quad - \frac{1}{2} y \bar{v}_{yy}(\gamma + y F, y, t) (F + y F_y)\end{aligned}$$

QED

Problem 6, (a) The vortex at $(x, y) = (0, a)$ has velocity

$$u_+ = \frac{\kappa(y-a)}{x^2 + (y-a)^2}, \quad v_+ = \frac{-\kappa x}{x^2 + (y-a)^2}$$

while the vortex at $(x, y) = (0, -a)$ has velocity

$$u_- = \frac{-\kappa(y+a)}{x^2 + (y+a)^2}, \quad v_- = \frac{\kappa x}{x^2 + (y+a)^2}.$$

The vortex at $(x, y) = (0, a)$ feels the velocity of the other vortex, which is

$$u_-(0, a) = \frac{-\kappa}{2a}, \quad v_-(0, a) = 0$$

On the other hand, the vortex at $(x, y) = (0, -a)$ feels the velocity of the first vortex, which is

$$u_+(0, -a) = \frac{-\kappa}{2a}, \quad v_+(0, -a) = 0.$$

Thus, the pair of vortices are mutually advected with the velocities

$$u_{\text{vort}} = \frac{-\kappa}{2a}, \quad v_{\text{vort}} = 0$$

and move parallel to the x -axis together.

(b) When the point vortices are located at $(x, y) = (u_{\text{vort}} t, \pm a)$, then the resultant velocity at all other points is given by

$$u = \frac{\kappa(y-a)}{(x-u_{\text{vort}} t)^2 + (y-a)^2} - \frac{\kappa(y+a)}{(x-u_{\text{vort}} t)^2 + (y+a)^2}$$

$$v = \frac{-\kappa(x-u_{\text{vort}} t)}{(x-u_{\text{vort}} t)^2 + (y-a)^2} + \frac{\kappa(x-u_{\text{vort}} t)}{(x-u_{\text{vort}} t)^2 + (y+a)^2}$$

In particular, at $y=0$

$$v(x, 0, t) = \frac{-\kappa(x-u_{\text{vort}} t)}{(x-u_{\text{vort}} t)^2 + a^2} + \frac{\kappa(x-u_{\text{vort}} t)}{(x-u_{\text{vort}} t)^2 + a^2}$$

$$\equiv 0.$$

Thus, we see that the velocity in the upper half-plane satisfies the no-flow-through condition at $y=0$. The vortex in the lower half-plane is the so-called image vortex required to enforce that condition for the flow in the upper half-plane.

(c) Since vortices are material points in 2D, adding the uniform velocity U changes the velocity of both vortices to

$$u_{\text{vort}} = U - \frac{\kappa}{2a}$$

Using this new definition of U_{vort} , we then obtain

$$u = U + \frac{\kappa(y-a)}{(x-U_{\text{vort}}t)^2 + (y-a)^2} - \frac{\kappa(y+a)}{(x-U_{\text{vort}}t)^2 + (y+a)^2}$$

$$v = \frac{-\kappa(x-U_{\text{vort}}t)}{(x-U_{\text{vort}}t)^2 + (y-a)^2} + \frac{\kappa(x-U_{\text{vort}}t)}{(x-U_{\text{vort}}t)^2 + (y+a)^2}.$$

(d) The streamwise velocity on the boundary $y=0$ now becomes

$$u = U - \frac{2\kappa a}{(x-U_{\text{vort}}t)^2 + a^2}$$

Note that

$$\alpha = \frac{U_{\text{vort}}}{U} = 1 - \frac{\kappa}{2aU}$$

$$\implies \kappa = 2aU(1-\alpha)$$

Thus,

$$\frac{u}{U} = 1 - \frac{4a^2(1-\alpha)}{(x-U_{\text{vort}}t)^2 + a^2}, \quad U_{\text{vort}} = \alpha U.$$

As long as $\alpha < \frac{3}{4}$, then $a^2(1-\alpha) > 0$ and we see that the most negative value is achieved for $x = U_{\text{vort}}t$ where

$$\frac{|u|_{\text{max}}}{U} = 4(1-\alpha) - 1 > 0.$$

Problem 7. (a) Noting that $U^2 = \mathbf{U} \cdot \mathbf{U}$, we see that

$$\nabla\left(\frac{1}{2}U^2\right) = U_j \nabla U_j \quad (\text{sum over repeated } i)$$

However,

$$\partial_i U_j = \partial_i (\partial_j \phi) = \partial_j (\partial_i \phi) = \partial_j U_i$$

is symmetric in i, j (i.e. there is no vorticity for potential flow!). Thus

$$U_j \partial_i U_j = U_j \partial_j U_i = (\mathbf{U} \cdot \nabla) U_i$$

and

$$\nabla\left(\frac{1}{2}U^2\right) = (\mathbf{U} \cdot \nabla) \mathbf{U}.$$

(b) From the Bernoulli equation we obtain

$$-\nabla P = \nabla\left(\frac{1}{2}U^2\right) = (\mathbf{U} \cdot \nabla) \mathbf{U}$$

by part (a). This, of course, is just the stationary Euler equation! Now substituting $\mathbf{U} = U \mathbf{t}_s$ and noting that $\mathbf{t}_s \cdot \nabla = \frac{\partial}{\partial s}$ gives

$$\begin{aligned} -\nabla P &= U \frac{\partial}{\partial s} (U \mathbf{t}_s) \\ &= U \frac{\partial U}{\partial s} \mathbf{t}_s + U^2 \frac{\partial \mathbf{t}_s}{\partial s} \end{aligned}$$

Now, using the Frenet-Serret equation

$$\frac{\partial \mathbf{t}_s}{\partial s} = \kappa_s \mathbf{n}_s$$

and $U \frac{\partial U}{\partial s} = \frac{\partial}{\partial s} \left(\frac{1}{2} U^2 \right)$, we get finally that

$$-\nabla P = \frac{\partial}{\partial s} \left(\frac{1}{2} U^2 \right) \mathbf{t}_s + U^2 \kappa_s \mathbf{n}_s.$$

(c) Assuming continuity of the pressure gradient across the thin boundary layer, we calculate the Lighthill source at the wall surface as

$$\boldsymbol{\sigma} = -\mathbf{n} \times \nabla P = \frac{\partial}{\partial s} \left(\frac{1}{2} U^2 \right) \mathbf{n} \times \mathbf{t}_s + U^2 \kappa_s \mathbf{n} \times \mathbf{n}_s$$

Since \mathbf{t}_s is, by definition, the streamwise direction, then $\mathbf{n} \times \mathbf{t}_s$ is the spanwise direction and the term $\propto \frac{\partial}{\partial s} \left(\frac{1}{2} U^2 \right)$ creates spanwise vorticity. On the other hand, if the streamlines bend in a direction perpendicular to both \mathbf{n} and \mathbf{t}_s , e.g. to pass around an obstacle in the flow, then

$$\boldsymbol{\sigma} \cdot \mathbf{t}_s = U^2 \kappa_s (\mathbf{n} \times \mathbf{n}_s) \cdot \mathbf{t}_s \neq 0$$

and the term $\propto U^2 \kappa_s$ can thus generate streamwise vorticity.